

Maximum Beam Current as a Function of Cavity Gradient and Detuning with a 3.8 kW RF Source

LCLS-II TN-15-29

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1 Introduction

L-band RF power for the SCRF cavities of LCLS-II will be provided by solid-state amplifiers (SSAs) for which the engineering specification calls for a maximum CW output power of 3.8 kW for the initial phase of operation. This figure is based on supporting a nominal design gradient of 16 MV/m at a maximum beam current of 100 μ A (see Engineering Note LCLSII-2.4-EN-0431). It takes into account waveguide losses, the nominal cavity coupling, operational overhead and up to 10 Hz cavity detuning. Note that there will likely be additional overhead – in the most recent (7/21/15) linac design schematic, 4 GeV is reached without exceeding 15.7 MV/m in L1-L3 and the beam runs off-crest in many cavities. Also, the beam current will likely be closer to 65 μ A.

In this brief note, we evaluate one aspect of flexibility in operational parameter space. In particular, we determine what limit our available RF power places on beam current as a function of the 1.3 GHz cavity gradient, which in turn can be used to compute the maximum beam energy for a given current. Results are shown for different levels of allowed detuning of the cavities (e.g., from microphonics).

2 Maximum Operating Current

Table 1 lists parameters of the 1.3 GHz accelerator cavities and the RF source relevant to the calculation.

Drive frequency	$f_0 = 1.3 \text{ GHz}$
Cavity length	<i>L</i> = 1.038 m
Effective R/Q	$R/Q = 1,010 \ \Omega$
Loaded quality factor	$Q_L = 4.12 \times 10^7$
RF source power	$P_{g} = 3.8 \text{ kW}$
Transmission efficiency	$\eta_{tr} = 0.918$
Overhead factor	OF = 1.08
Power available to cavity	$P_i = 3.26 \text{ kW}$

TABLE 1: Cavity and RF Parameters

The power required by an SCRF cavity to sustain a given voltage with a given beam current riding on crest and a resonance detuning amplitude δf (i.e. $f_c = f_0 + \delta f$) is given by the following equation.

$$P_{i} = \frac{V_{c}^{2}}{4\frac{R}{Q}Q_{L}} \left[\left(1 + \frac{I_{b}}{V_{c}}\frac{R}{Q}Q_{L}\right)^{2} + \left(2Q_{L}\frac{\delta f}{f_{0}}\right)^{2} \right]$$
(1)

Inverting this for the maximum current that can be accelerated at a given cavity voltage with fixed power and a fixed external coupling yields

$$I_{b,\max} == \frac{V_c}{\frac{R}{Q}Q_L} \left[2Q_L \sqrt{\frac{R/Q}{Q_L} \frac{P_i}{V_c^2}} - \left(\frac{\delta f}{f_0}\right)^2} - 1 \right].$$
(2)

This beam current limit is plotted in Fig. 1 vs. the cavity gradient (= V_c/L) for different detuning values assuming the cavity input power equals the RF source power derated by the transmission loss and operational overhead. By design, a detuning of 10 Hz limits the current to 100 μ A at 16 MV/m. At 15.7 MV/m, the current can be as high as 110 μ A, and a 65 μ A beam can be accelerated as high as 17.1 MV/m. Current and gradient do not scale inversely because, with fixed over-coupling (Q_L), only a fraction of the power goes into the cavity.



Figure 1. On-crest beam current limit as a function of acceleration gradient for a 3.8 kW RF source and cavity detunings of 10 Hz (blue), 5 Hz (green) and 2 Hz (red). The dashed black is the asymptote for perfect tuning, and the asterisk indicates the parameters for which the source power was specified.